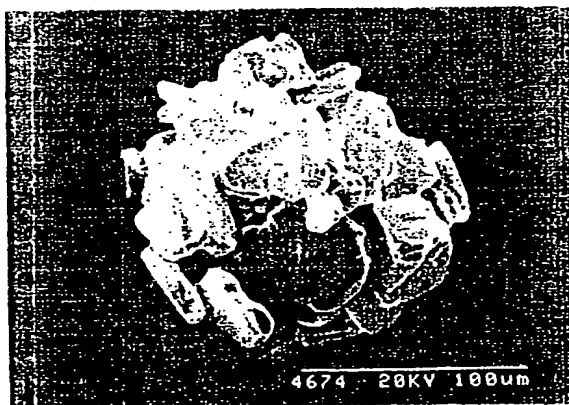


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(54) Title: HIGH SPEED, HIGH QUALITY THREE DIMENSIONAL PRINTING**(57) Abstract**

A system for producing three dimensional components by bonding together successive layers of a porous material with droplets of a binder material. A binder printhead has an array of nozzles which controllably supply jets of binder material droplets to the layers of porous material. The printhead is scanned in a raster scan fashion over each layer of porous material along a first scan axis in one direction to provide first fast scanning paths of droplets. The printhead is then moved laterally of such one direction and is then moved along the fast scan axis in the opposite direction to provide second fast scanning paths of droplets which are interlaced with the first scanning paths. The supply of the droplets to the porous material can be controlled so as to control the overlapping thereof to produce various desired surface and interior characteristics of the components.

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High Speed, High Quality Three Dimensional Printing

Introduction

This invention relates generally to the production of components directly from a computer model by three dimensional printing techniques, using a layered process, and, more particularly, to the
5 production of components at a high rate in a manner such that the quality of certain properties of the components, and especially the surface finishes thereof, can be controlled.

Background of the Invention

10 Components can be created directly from a computer model using such three dimensional printing processes which can be defined as processes that construct objects in layers using a computer model of the objects. Exemplary processes of this type are described, for example, in U.S. Patent Application of Sachs et al., Serial No.
15 07/447,677, filed on December 8, 1989, which application is incorporated by reference herein. As described in such application, a component can be produced by spreading powder (or other porous material) in a layer and then depositing a further material, e.g., a binder material, at specific regions of a layer as determined by a computer
20 model of the component. The further material acts to bind the powder both within the layer and between layers. This process is repeated layer after layer until all layers needed to define the components have been printed.

25 The fundamental requirement that must be satisfied if three dimensional printing techniques are to be capable of manufacturing

large quantities of product is to simultaneously satisfy the need to produce components at high rate and with high quality. Control of the quality of the part includes the control of dimensions and the control of its surface finish. Another aspect of component quality control is the control of the internal structure of the component so as to yield certain desired properties thereof, including a desired isotropic nature of the part, or a desired anisotropic nature of the part.⁸⁴

The rate at which parts can be created in three dimensional printing processes can be understood by recognizing that, typically, each cubic centimeter of binder that enters the powder bed binds approximately 1 cubic centimeter of powder and creates a portion of the part of approximately 2 cubic centimeters in volume. Thus, the overall volume of a part created is roughly twice the volume of binder deposited, the total volume varying depending on the type of powder used, so that it can be more or less than twice the volume of binder deposited. The attainment of a high production rate in a three dimensional printing process thus depends on depositing the binder at a high volume flow rate.

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The binder can be applied using ink-jet printing techniques and the aforesaid Sachs et al. application describes a configuration of an apparatus where the device which delivers the binder is moved over the bed of porous material in a raster scan motion. Such configuration of a three dimensional printing machine, while not the only one possible, forms the principal basis for the invention described herein.

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When the binder is delivered using ink-jet printing techniques, each droplet of binder enters the powder bed and joins together a

number of powder particles to form a generally spherical "primitive" building element. FIG 1 shows a micrograph of an exemplary spherical "primitive" element which is about 120 microns in diameter. The primitive shown therein was made by printing a single 80 micron diameter droplet of binder into a bed of powder. The binder used was colloidal silica and the powder was an alumina powder having an average particle size of 30 microns. As successive droplets are deposited, these spherical building elements overlap to form the finished component. The surface finish of the finished part is largely determined by the placement of the individual droplets and how they overlap. FIG. 2 shows a portion of a component where five droplets, shown in a simplified diagrammatic fashion, have been printed with some, relatively small, overlap. In FIG 2, each of the circles represent diagrammatically a generally spherical building element of the type shown in FIG. 1 which results from an individual binder droplet. The surface of the printed part is defined by the surface 13, which can be seen to be somewhat rough due to the nature of the contours of the primitives. By contrast, FIG 3, shows diagrammatically a portion of a component comprising a plurality of spherical elements which have been printed with a higher degree of overlap with the result that the surface 15 is relatively smoother than the surface 13. The problem of creating high quality parts at a high production rate can be seen to be a problem of how to deposit droplets at a relatively high rate while retaining the ability to determine and control the location of the droplet placement.

The requirements for a high production rate with high quality in a three dimensional printing process provide a significantly different challenge than the conventional printing of ink on paper. One

significant difference is that in printing on paper it is the general practice to move the paper at high speeds past a stationary printhead. In three dimensional printing it is preferable, and often necessary, to move the printhead past a stationary bed of porous material because the bed of porous material is often relatively large and massive. Another difference is that, in conventional printing of ink on paper, the droplet separation needed to achieve high resolution printing is considered to be about 300 dots per inch (dpi). Thus, if the droplet position can be effectively controlled to occur at intervals of 1/300 inch, or approximately 85 microns, high resolution printing can be accomplished. However, such a 300 dpi droplet placement would be quite insufficient for the creation of three dimensional components. First, a 300 dpi placement would mean that the dimensions of the three dimensional object could only be controlled to within ± 85 microns. Second, the surface finish of the object would be quite rough. For example, if the primitives of FIG 2 represented primitives of 120 micron diameter and are placed 85 microns apart, the resulting surface would have a root-mean-square (RMS) roughness of approximately 6.0 microns and would result in a fairly rough surface. In fact, then the creation of components and surfaces in three dimensional printing processes is more complex than the situation represented by FIGS. 2 and 3 in that it is a 3-D problem, while conventional printing of ink on paper is a 2-D problem. Thus, in three dimensional printing, the placement of droplets must satisfy the requirement that the overlap between droplets must serve to bind together a self-supported component in three dimensions. In contrast, in conventional printing of ink on paper, only a 2-D image needs to be defined, and further, the paper itself provides the physical support for the image.

Brief Summary of the Invention

In order to achieve high quality printing at a high rate in accordance with the invention, a multiple array of on-off controlled nozzles is scanned over the surface of a bed of porous material in multiple passes using an interlacing of the printed lines which deposit the binder thereon.

A further method for achieving the fine drop placement resolution required is to utilize an array of proportionally deflected jets disposed so that at least a component of the deflection is perpendicular to the direction of fast scan of the raster. The use of proportional deflection permits the edges of an object to be contoured to create smooth surfaces or to create selected patterns which are used to fill the interiors of components.

The accuracy of drop placement is maintained by an on-line measurement of the position and velocity, or time of flight, of the jets so that an adjustment of the data file which defines the model of the component being made can be made to compensate for any changes that may be needed.

Detailed Description of the Invention

The invention can be described in more detail with the help of the accompanying drawings wherein

FIG. 1 shows a photomicrograph taken in a scanning electron microscope of an exemplary "primitive" element formed by the interaction of a single droplet of binder with powder;

5 FIG. 2 shows a diagrammatic illustration of the nature of a surface defined by the overlap of droplets in a three dimensional printing process where the overlap is relatively coarse;

10 FIG. 3 shows a diagrammatic illustration of the nature of a surface defined by the overlap of droplets in a three dimensional printing process where the overlap is finer than in FIG. 2;

15 FIG. 4 shows a schematic illustration of an exemplary on-off continuous-jet printhead;

 FIG. 5. shows a schematic illustration of an exemplary proportionally deflected continuous-jet printhead;

20 FIGS. 6(A) and 6(B) show an exemplary three dimensional printing pattern using an interlaced scan of an array of on-off jets;.

 FIGS. 7(A) and 7(C) show an exemplary three dimensional printing pattern using an array of proportionally deflected jets;

25 FIGS. 8(A) and 8(B) show an exemplary three dimensional printing pattern using an array of proportionally deflected jets. where the array is disposed at an angle with respect to the direction of fast scan of the printhead;

FIGS. 9(A), 9(B) and 9(C) show exemplary results when using proportional deflection techniques to create various edge contours of components;

5 FIGS. 10(A), 10(B) and 10(C) show exemplary patterns created using proportional deflection techniques to define various interior structures of components; and

10 FIG. 11 shows an exemplary structure for making time of flight measurements with a continuous-jet printhead, together with exemplary voltage waveforms used therefor.

15 In an exemplary embodiment of the invention, continuous-jet ink-jet printing technology is used to deliver the binder to the bed of porous material. Continuous-jet technology is known to the art and FIG. 4 shows a diagram of an exemplary continuous-jet structure where the control of the droplets supplied therefrom is arranged to the controlled in an on/off manner. A pressurized fluid is emitted from a nozzle 19 in a continuous stream 22. Piezo-ceramic element 21
20 causes nozzle 19 to vibrate at a selected frequency so as to promote the breakup of the stream into droplets 24. The breakup happens at a particular position 26 along the length of the stream which is arranged to occur within a charging cell 23. When a voltage is applied to the charging cell to produce a voltage between the slightly conductive
25 stream of liquid 22 and the charging cell, the droplets acquire a capacitively induced charge. When charged droplets 27 enter the high electric field between plates 25, the electric field being created by a constant voltage applied across such plates, the droplets are deflected and caught by a catcher element 29 and removed from the printhead.

When no voltage is applied between the conductive stream of liquid and the charging cell, the droplets 31 are not charged and travel straight through and proceed to the target. In this manner, a continuous-jet printhead can be turned on and off by turning the voltage applied to the charging cell on and off. Since the charge on the droplets depends on the voltage applied between the droplet stream and the charging cell at the moment of break-off, the droplets may be individually controlled.

Continuous-jet printing may also be practiced in a proportional deflecting mode where the jet is deflected through a range of positions in order to deliver droplets at specified locations. In FIG. 5, for example, a sinusoidal voltage is applied to a charging ring 23 with the result that successive droplets are charged by different amounts in a sinusoidally varying pattern. As these droplets enter deflection plates 25, they are deflected by an amount proportional to their charge. It should be noted that droplets can be charged either positively or negatively, resulting in deflections on both sides of a line 35 which would be traveled by uncharged droplets. Controlling the voltage at the moment of break-off therefore allows for control of the landing position of the droplet. Applying a large voltage at the moment of break-off will cause a droplet to be deflected into a catcher element 29 as in the case of the on-off printhead of FIG 4.

One aspect of the current invention is to provide for precise drop placement with high deposition rates utilizing arrays of ink-jets, such as an array of binary continuous jets in a single printhead structure. In this embodiment, the printhead is scanned back and forth over the surface of the powder bed. Linear arrays of such binary continuous

jets can be fabricated with nozzle spaces as small as 100 microns. Such linear arrays are fabricated by Diconix/Kodak Corporation of Dayton, Ohio. While arrays of such spacing are satisfactory for moderate resolution printing of ink on paper, 100 micron drop
5 placement resolution is insufficient for three dimensional printing. In order to provide the drop placement resolution needed for high quality three dimensional printing, in accordance with the invention, multiple passes of the printhead are made over the surface of the powder bed using an interlacing of the binder print lines as shown in FIG. 6(A) and
10 FIG. 6(B). In a typical application, a printhead structure having a linear array 53 of eight 50 micron diameter nozzles with 100 micron spacing between nozzles can be employed. In FIG. (6A), the printhead is shown scanning from left to right over a bed 51 of porous material. Tracks 55 depict the impact areas of the deposited binder droplets.

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In FIG 6(B) the printhead 53 is shown as having been moved downward by one-half a nozzle spacing and then moved to scan from right to left. Tracks 57 depict the impact areas of both the left to right and the right to left passes of the printhead.

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In a typical application, it would be necessary to scan the printhead over the surface of the powder at a very high rate in order not to provide excessive binder to the powder bed which would result in an undesired bleeding of the binder in the powder. For example, if a
25 layer of 200 microns thickness were being printed, the desired amount of binder per unit of deposition would be approximately $0.01 \text{ cm}^3/\text{cm}^2$. This amount of binder would fill up the void space in a bed of powder for a typical void space of 50%. Typically, the stream exiting from a 50 micron diameter nozzle would create 80 micron droplets at a rate of

approximately 60 kilohertz. If the nozzle spacing is 100 microns and one interlacing pass is made, as shown in FIG. 6(B), the printhead would have to traverse at a speed of approximately 3.0 meters/second. This speed would result in the deposition of droplets at spacings of 50 microns along the direction of fast axis travel. Droplets would then be deposited on a roughly square array of 50 microns on a side, leading to material properties that are similar in the two directions within a printed layer. If the speed were lower than 3.0 meters/sec and all droplets were printed, too much binder would be deposited and bleeding would result. Alternatively, a lower traverse speed could be used if not all droplets were printed. A similar interlaced raster pattern could be created with a printhead that delivered droplets with on-off control by drop-on-demand printhead technology.

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Another embodiment of the current invention utilizes an array of proportionally deflected jets. In this case, the array of proportionally deflected jets is again scanned back and forth over the surface of the powder bed. The proportional deflection of the jet allows for a precise placement of the droplets in the powder bed. FIG. 7(A) shows an exemplary printhead structure 61 having a linear array of four nozzles 63 oriented perpendicular to the direction of fast scan of a raster pattern over a print area 69. Each jet is located within a set of deflection plates 65 so that the jet may be proportionally deflected along the direction of the linear array and perpendicular to the direction of fast scan of the printhead. The polarity of the plates 65 is alternated with the result that the electric field, represented by arrows 67 alternates between adjacent plates. Typically, the jet diameter might be 50 microns and the jets might be 3 millimeters apart. It is

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understood that for the purposes of illustration only, the scale used in FIG. 7(A) is not exact, but is meant to show that the spacing between jets is typically much larger than the jet diameter. Because of the need to dispose the jets between a pair of plates 65, it is difficult to have
5 the spacing between jets very much smaller than 3 millimeters.

The deflection of the jets can be such as to cover the full range of distance between adjacent jets so that the entire area 69 can be printed with one pass. However, when a jet is deflected through a
10 relatively large angle, errors in jet deflection can be difficult to control. These errors include both aerodynamic errors and electrical errors relating to the charging of the droplets. Thus, it is preferable, in accordance with the invention, to use only a relatively small amount of deflection of the jet so as to retain good accuracy in the droplet
15 placement. In such a case, a single pass of the printhead does not cover the full area so that an interlacing scan pattern is needed. As an example, a single jet might be deflected so as to cover a printing area of 200 microns in width, so that 15 interlaced patterns would then allow for a complete printing of areas with an array having a 3 mm jet
20 spacing. FIG. 7(B) shows the printhead 61 traveling from left to right, each proportionally deflected stream covering a relatively narrow path 71 as the printhead travels. FIG. 7(C) shows the printhead having been displaced downward and traveling from right to left and depositing binder over the lower portion of the path 73. It should be
25 noted that the deflection can be to both sides of the position defined by an uncharged droplet, as was discussed in the context of FIG 5. Alternatively, the deflection can be just to one side of the position defined by an uncharged droplet. In the latter case, it is possible to

configure the printhead to catch uncharged droplets, while in the former case, uncharged droplets will be printed.

5 The use of proportional deflection allows for very fine control over the drop placement position in a direction perpendicular to the direction of fast scan of the raster. Another advantage of the use of proportional deflection is that the scanning speed of the printhead can be substantially reduced. This has the beneficial effect of providing finer resolution of drop placement along the direction of fast scan of the raster as well as making the equipment easier to fabricate. The finer resolution along the fast axis may be understood by noting that the requirement for 3-D printing is to deposit a specified amount of binder per unit area of printing for any particular layer thickness. As the binder droplets are displaced lateral to the fast axis, an individual stream covers more area. As a result, the fast axis can be slowed down. Since the droplet generation rate for a given nozzle configuration is fixed, a slower fast axis travel results in a higher number of droplets per unit length along the fast axis with the consequence of providing finer resolution.

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Other configurations of arrays of proportionally deflected jets are possible. FIG. 8(A), for example, shows a printhead structure 81 having an array of five jets 91 which is mounted at an angle with respect to the fast axis of scanning. The advantage of such an approach is that it eliminates the need for a high voltage deflection plate to be disposed between each nozzle. Rather, a single set of plates 83 can serve all nozzles and cause a deflection indicated by arrow 87 which is perpendicular to this set of plates. This deflection is at an angle, typically 45 degrees, with respect to the direction of fast

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axis scan indicated by arrow 85. The deflection thus has a vectorial component which is perpendicular to the direction of fast axis scan and, therefore, by appropriate computation can be set up to create a wide variety of patterns. FIG. 8(B) shows the printhead 81 as it scans across a print area 93 leaving binder print tracks 89. A further advantage of this approach is that the jets in the array can be relatively closely spaced and, therefore, fewer interlaced scanning lines (and, in some cases no interlaced scan lines) would be needed to cover the entire print area than would be needed, for example, in the arrangement shown in FIGS. 7(A), 7(B) and 7(C).

One effective application of the aspect of the invention is to use proportional deflection in order to create smooth edges on components. FIG. 9(A) shows the edge definition that would be obtained using an on-off printhead, (i.e., without proportional deflection) with a droplet spacing of 50 microns in both directions. It should be noted that in attempting to create the part contour 101, the attainable resolution of droplet placement causes significant steps, or discontinuous 103 to appear in the edges of the part. FIG. 9(B) shows a smooth edge that can be created using proportional deflection techniques. In this case a single scan line 105 is shown. It should be noted that the spacing of droplets along the scan line is smaller in the proportionally deflected case of FIG. 9(B) than in the on-off case of FIG. 9(A). Some of the droplets 107 are used to create the smooth edge contour itself, while some of the droplets 109 are used to fill in the area of the binder print line defined by one pass of the jet. For clarity, FIG. 9(C) shows only those droplets 107 which have been used to create the smooth edge contour.

Another application of the invention is to use proportional deflection to create desired patterns and properties within the interior of the body of a component. FIG. 10(A) shows two different patterns that may be created within the body of a component by using

5 proportional deflection to position the droplets. The patterns are each created around scan lines 123 within the printing area 121. It should be noted that no reduction in printing speed is needed to accomplish this droplet placement when using proportional deflection. Some patterns may be useful for creating deliberately isotropic properties

10 within the component, while other patterns may be useful for creating deliberately anisotropic properties within the component. The degree of proportional deflection may even be selected by a random number generator to create unique part properties. FIG. 10(B) shows a pattern which utilizes relatively little overlap between adjacent droplets of a

15 layer. Such patterns are useful when considering that the part is actually three dimensional and thus successive layers also display overlapped characteristics. Thus, it may be desired to minimize the overlap within a layer and to make use of greater overlap between layers to create certain desired properties of the part. One example is

20 to deposit the droplets in a pattern that results in a placement of the droplets in the three dimensional part in a hexagonal closely-packed lattice array. Such a lattice array is familiar in the art of crystallography as an array which produces the highest packing of uniform sized spheres. The use of such a lattice array would be useful

25 in creating parts with isotropic properties based on overlap in all three dimensions of the part. Further, it is possible to create parts that have no overlap between printed droplets within a plane, or layer, but which relies on the overlap between planes or layers to define a component. FIG. 10(C) shows a pattern that can be used to create a cellular

structure within a component. In FIG. 10(C) the proper relationship between two adjacent lines of proportionally deflected droplets defines the cellular pattern within the component.

5 One problem that can arise when using continuous jet printheads is that certain changes in the binder stream over time can cause inaccuracies in the placement of droplets. These changes can be of two types. First of all, changes in the direction of the jet as it exits the nozzle can cause different landing positions of the droplets.

10 Secondly, even if there is no change in the direction of the emerging jet, changes in the exit velocity of the stream can also cause changes in the landing position of droplets. This is because there is typically a 2 cm distance between the exit from the nozzle tip and the impact point on the porous bed. Also, typically the downward velocity of the

15 jet is 10 m/sec and the lateral velocity is 2 m/sec. Thus, the droplet follows a trajectory where it impacts the powder bed at an angle and a change in the jet exit velocity will change the distance "downstream" that the droplet impacts. Accordingly, one aspect of the invention is to measure changes in both the stream angular position and the stream

20 velocity, on-line in the machine, and to take corrective action based on these measurements so as to maintain overall drop placement accuracy.

 Changes in jet position, i.e., the angular position of the jet

25 stream, can be measured using optical techniques. For example, two CCD line cameras can be used to image the position of the stream, i.e., the jet position in two orthogonal directions, either when the printhead is at rest or when it is in motion, so that changes therein can be measured. In a three dimensional printing machine, such

measurements might be taken while the machine is spreading the next layer of porous material. Changes in the stream velocity can be measured using any one of a variety of methods of flow rate measurement, e.g., including the measurement of pressure drop
5 through a known restriction, and other techniques.

One particularly useful method in accordance with the invention is to directly measure changes in the time of flight of the droplets, that is the time between the moment of detachment from the stream and
10 the moment of impact at the powder surface as illustrated in FIG. 11. The time of flight is the true parameter of interest (as opposed to the stream velocity) because the time of flight takes into account deceleration of the droplets as they travel to the powder. The time of flight may be measured by imposing a regular varying voltage, such as
15 a sinusoidal voltage, at the charging cell 131 of a continuous-jet printhead, thereby imposing a sinusoidally varying charge on successive droplets 137. A wire or other conductive body 135, is appropriately carried by the printhead or is otherwise suitably positioned, at the level of the porous bed at a distance 133 from
20 charging cell 131. The wire 135 acts as a capacitive pickup and yields a sinusoidally varying voltage which has a phase delay with respect to the sinusoidally varying voltage imposed at the charging cell 131. This phase delay may be used to provide a measurement of the time of flight. Typically, for a stream with an exit velocity of 10 m/sec and a
25 droplet generation rate of 60 kilohertz and a flight distance 133 of 2 cm, the imposed sinusoidally varying voltage has a frequency between 200 and 1000 Hertz.

The measurement of time of flight, or any measurement of velocity, can be used to adjust the time of flight or velocity in a closed loop control system by modulation of the pressure driving the jet. For example, if the measured time of flight is higher than the desired time
5 of flight, the pressure can be increased so to increase the jet velocity and decrease the time of flight. However, it will be understood that typically in a multiple nozzle printhead, no separate adjustment is possible for each of the velocities of the many jets and, hence, only the average velocity is used for such adjustments in a closed loop
10 fashion.

The measurements of changes in jet position and either jet velocity or time of flight, as discussed above, must be used to correct for the accurate drop placement of each jet individually as no one
15 correction will account for all the separate changes of the jets. The measurement of changes in jet position can be combined with a measurement in the change of time of flight by recognizing that an increase in the time of flight means that the droplet will travel further along the direction of fast scan of the raster before impacting on the
20 powder bed. For example, if the time of flight is 2.0 msec and the fast axis scan speed is 1.0 m/s, the droplets will move 2mm along the direction of fast scan of the raster as they fly from the point of detachment from the continuous-jet to the powder surface. If the time of flight should increase to 2.1 msec, there will be a shift in droplet
25 landing position of 0.1 mm. This shift is functionally equivalent to a shift of 0.1 mm which would result from a change in the angular position of the jet. Thus, knowing the change in time of flight and the printhead traverse speed, the effect of the change in time of flight can

be added to the measured change in jet position. These position changes may now be corrected for.

When the position of a jet changes so that the impact point moves along the direction of fast scan, the release point can be adjusted so that the impact takes place at the intended spot. This is accomplished by electronically advancing or retarding the information in the data file that defines the component model which information is supplied to the printhead as it travels along the direction of fast scan. For example, if the projected impact is further down the fast scan than desired, the information can be electronically advanced so that the actual impact is as desired. Referring to FIG. 7, when the position of a jet changes so that the impact point moves lateral to the direction of fast scan, the degree of proportional deflection may be changed by electronic control so as to cause the true impact at the desired location. Thus, by the combination of advancing/retarding information to the printhead and changing the amount of proportional deflection, the measured jet position and time of flight can be used to provide corrective actions to maintain drop placement accuracy.

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While the particular embodiments of the invention represent preferred embodiments thereof, modifications may occur to those in the art within the spirit and scope of the invention. Hence, the invention is not to be construed as limited to the particular embodiments described herein, except as defined by the appended claims.

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What is claimed is:

1. A system for producing a three dimensional component by bonding together successive layers of a porous material with droplets of a binder material, said system comprising

a binder printhead having an array of nozzles for supplying jets of binder material droplets to selected regions of said layers of powder material;

means for controlling the supplying of said jets of droplets;

means for moving said printhead in a raster scan fashion over a layer of said porous material so that during each scan said printhead is moved along a fast-scan axis in one direction to provide a first plurality of fast-scanning paths of said droplets, is moved laterally with respect to said fast-scan axis following the movement of said printhead in said one direction, and is moved along said fast-scan axis in the opposite direction after the lateral movement thereof to provide a second plurality of fast-scanning paths of said droplets which are interlaced with said first plurality of fast-scanning paths.

2. A system in accordance with claim 1 wherein said controlling means controls the supplying of droplets from said array of nozzles in an on-off manner.

3. A system in accordance with claim 1 wherein said controlling means controls the supplying of droplets so as to proportionally deflect said droplets which are supplied from said array of nozzles.

4. A system in accordance with claim 3 wherein said array of nozzles is a linear array thereof which is arranged so as to be perpendicular to the direction of said fast-scan axis and further including a plurality of deflection plates, each of said nozzles being positioned between a pair of said deflection plates.

5. A system in accordance with claim 4 wherein the distance separating said nozzles in said linear array is substantially larger than the diameter of said nozzles.

6. A system in accordance with claim 5 wherein the controlling means controls the proportional deflection of said droplets so that the deflection thereof is large enough to cover substantially the entire distance between each first scanning path of said droplets so that a selected region of said layer of porous material can be completely covered by said droplets by controlling the movement of said printhead so that the printhead moves along said fast-scan axis only in said one direction but not in said opposite direction.

7. A system in accordance with claim 5 wherein the controlling means controls the proportional deflection of said droplets so that the deflection thereof is relatively small so that the moving of said printhead along said fast-scan axis in said one direction and in said opposite direction must be repeated a number of times to completely cover a selected region of said layer of porous material with said droplets.

8. A system in accordance with claim 3 wherein said controlling means controls the proportional deflection of said droplets

on to the layer of porous material at which the edges of the component are to be formed so that overlapping of the positions of said droplets on said layer is such as to provide smooth surface contours at said edges.

9. A system in accordance with claim 3 wherein said controlling means controls the proportional deflection of said droplets on to the layers of porous material at which the interior portions of the component are to be formed so that the overlapping of the positions of said droplets on said layers is such as to provide a selected pattern of said bonded porous material within the interior of the component.

10. A system in accordance with claim 9 wherein said controlling means controls the overlapping of said droplets so as to produce an isotropic pattern with the interior of said component.

11. A system in accordance with claim 9 wherein said controlling means controls the overlapping of said droplets so as to produce an anisotropic pattern within the interior of said component.

12. A system in accordance with claim 9 wherein the controlling means controls the overlapping of said droplets so as to produce a cellular structure within the interior of said component.

13. A system in accordance with claim 3 wherein the controlling means controls the overlapping of said droplets so as to produce substantially little or no overlapping of droplets in the layers of said porous material and to produce overlapping of droplets between the layers of said porous material.

14. A system in accordance with claim 1 and further including means for making measurements of changes in the positions of said jet droplets and changes in the velocities of said jet droplets or in, the times of flight of said jet droplets from the time at which they are formed at the nozzles of said array to the time at which they impact on to the layer of porous material, said control means responding to said measurements to control the placements of said jet droplets on said porous material.

15. A system in accordance with claim 14 wherein said control means controls the supplying of said jet droplets in accordance with information supplied to said control means from a data file which defines a model of said component and in accordance with the proportional deflections of said droplets from said nozzles, said control means responding to said measurements to advance or retard the supplying of said information to said control means and to control the amount of said proportional deflections to correct for inaccuracies in the placements of said droplets on said porous material.

16. A system in accordance with claim 14 wherein the means for making measurements of changes in the time of flight of said droplets includes

means for charging said droplets as they are formed;

means for imposing a periodic voltage on said charging means to produce charges on said droplets as they are formed;

means for determining a first phase of said periodic charging voltage when it is imposed on said charging means;

means for determining a second phase of said periodic charge voltage on said droplets when they impact on to said layer of porous material;

means for determining the difference between said first and second phases to provide a measurement of the time of flight of said droplets.

17. A system in accordance with claim 16 wherein said measuring means imposes a sinusoidally varying voltage signal on said charging means.

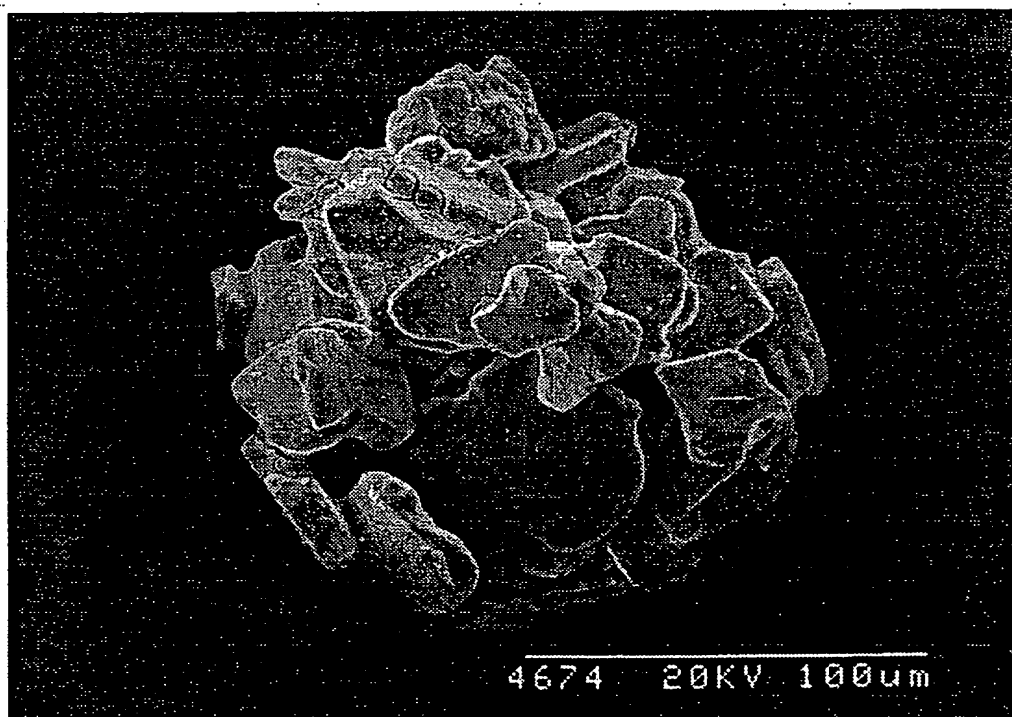


FIG. 1

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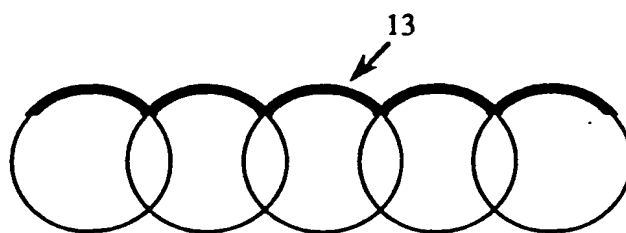


FIG. 2

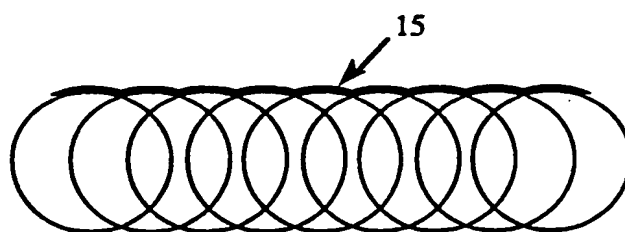


FIG. 3

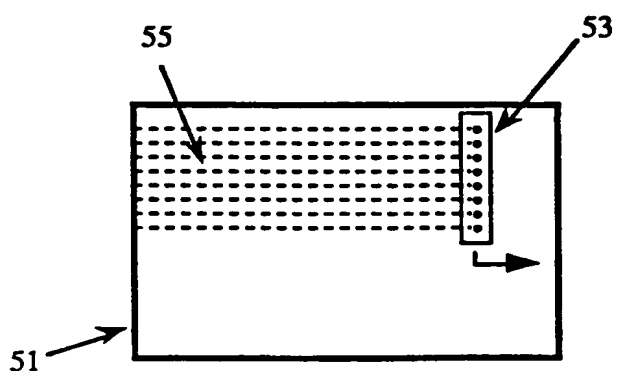


FIG. 6(A)

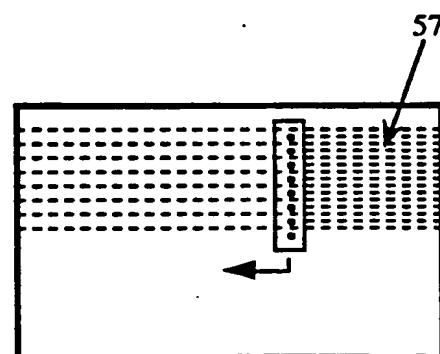


FIG. 6(B)

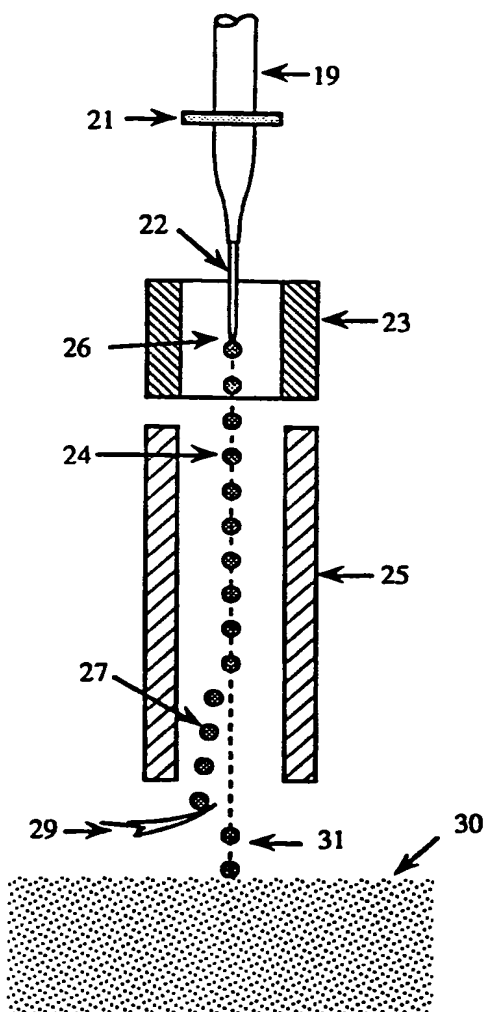


FIG. 4

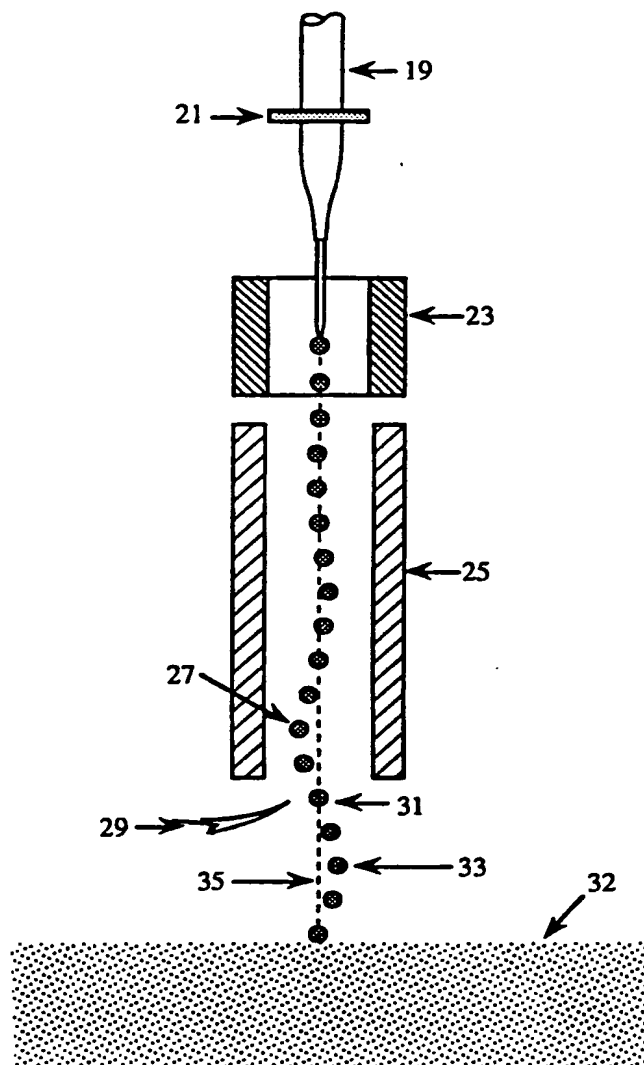


FIG. 5

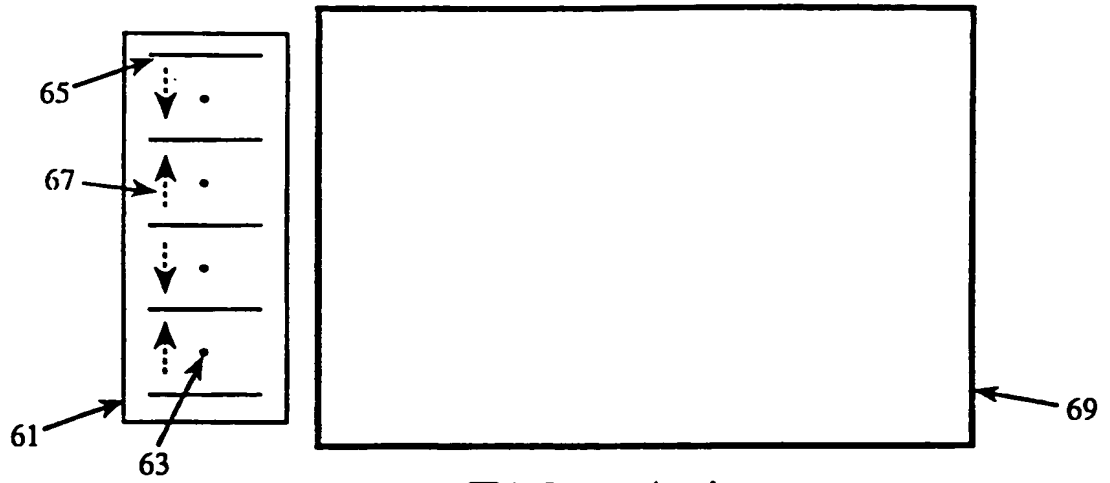


FIG. 7(A)

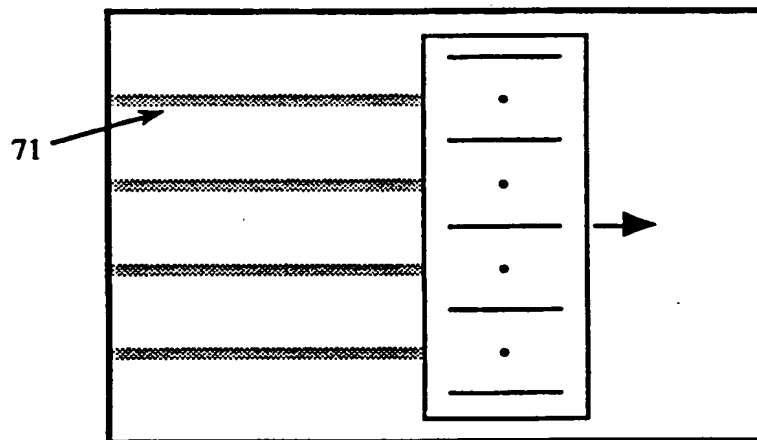


FIG. 7(B)

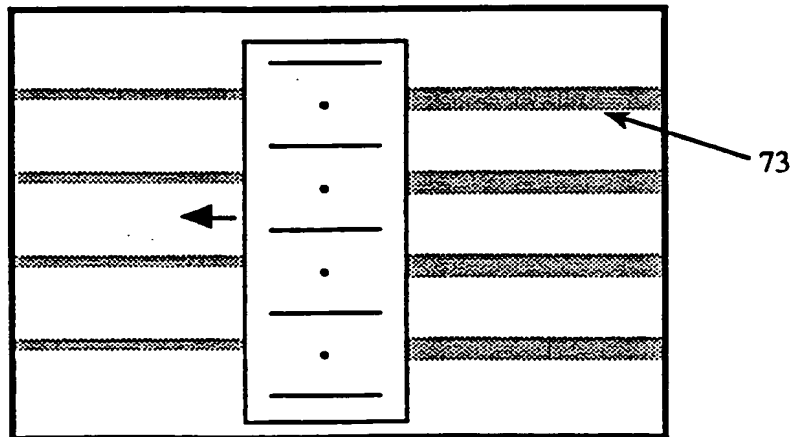


FIG. 7(C)

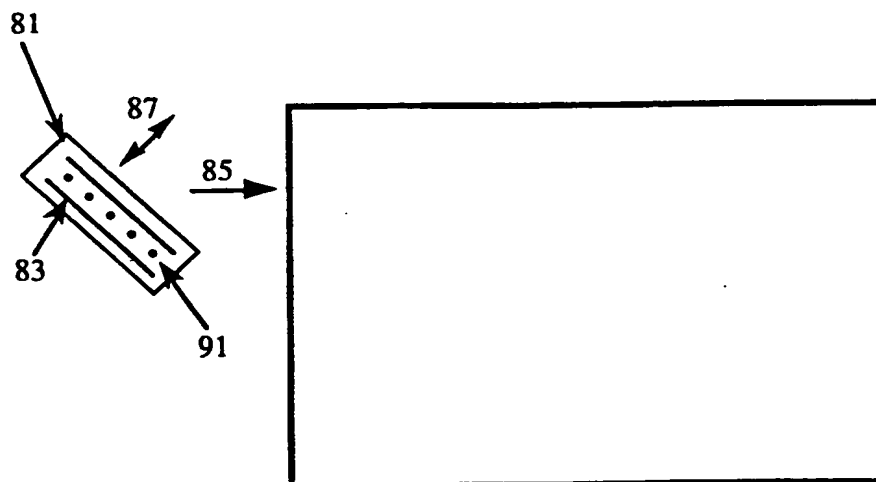


FIG. 8(A)

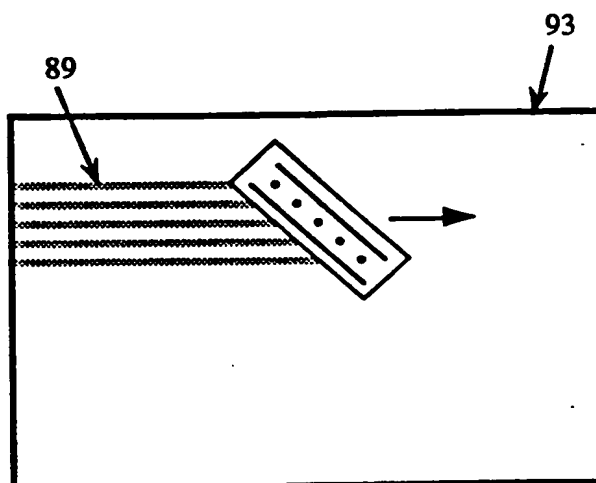


FIG. 8(B)

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FIG. 9(A)

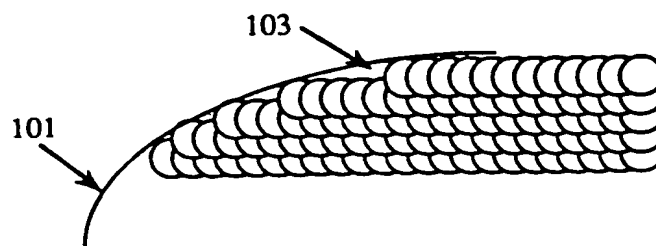


FIG. 9(B)

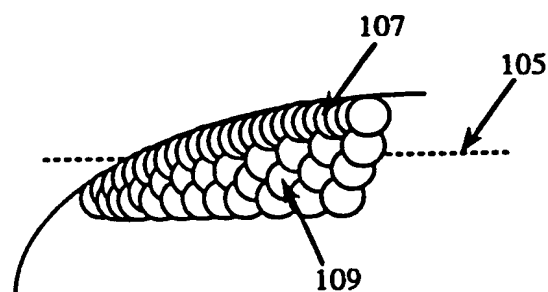


FIG. 9(C)

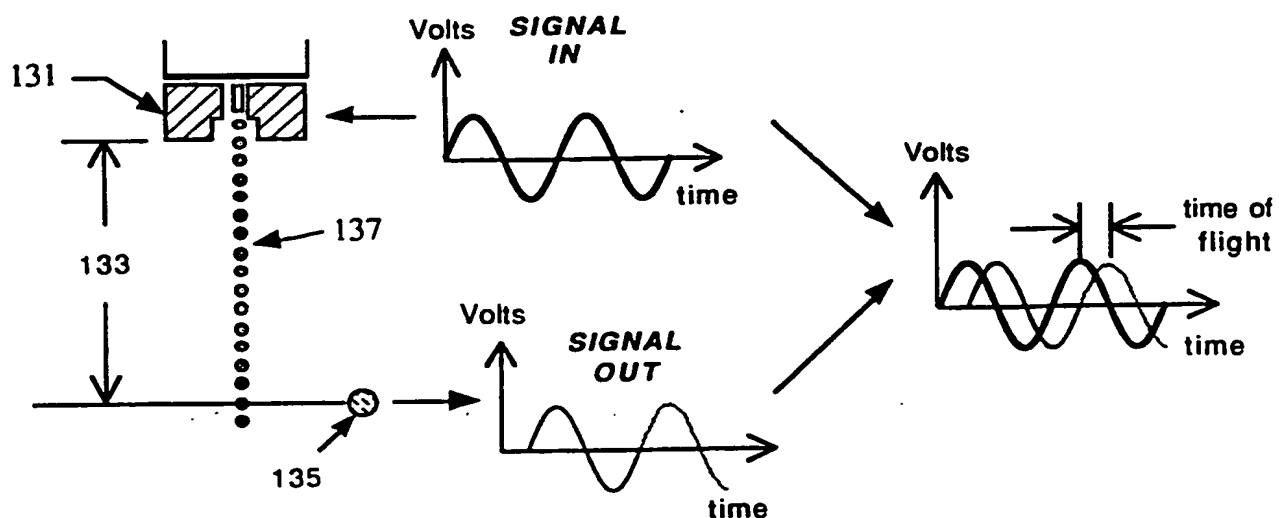
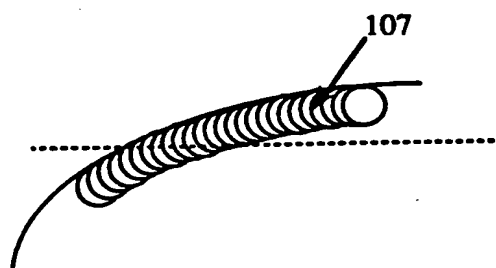


FIG. 11

SUBSTITUTE SHEET (RULE 26)

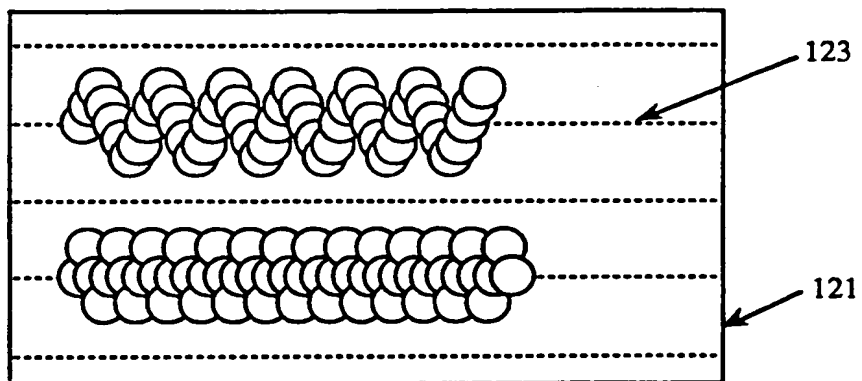


FIG. 10(A)

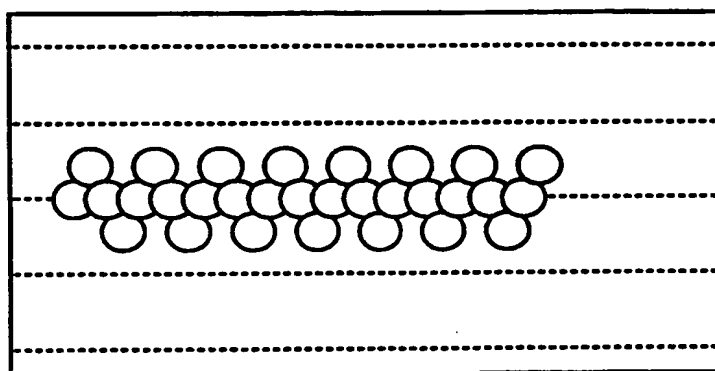


FIG. 10(B)

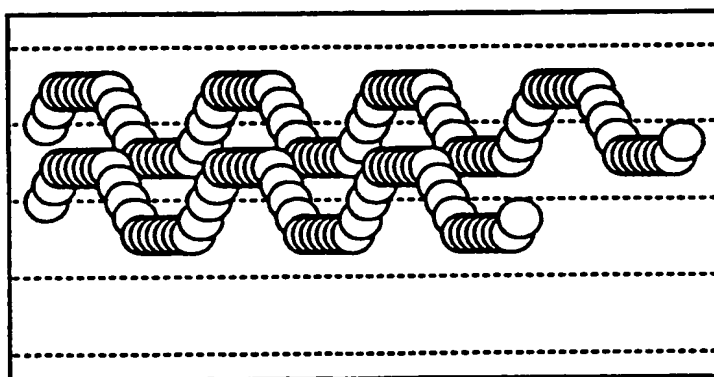


FIG. 10(C)